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Mechanically Stable, Stretchable Ferroelectric Thin-Film Transistors for Display Application

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Abstract

We present ferroelectric thin-film transistors (FE-TFTs) with a metal-insulator-semiconductor-ferroelectric (MISF) structure on polyimide (PI) and polydimethylsiloxane (PDMS) substrate. The memory window is 9.1 V and can operate under a 1 mm bending radius. Its biaxial stretchability is 30%. We proposed a 3T0C pixel circuit without a capacitor for the PWM mode of micro-LED displays using FE-TFTs.

Author Keywords

spray pyrolysis; ferroelectric thin-film transistor (FE-TFT); zirconium oxide (ZrO₂); flexible & stretchable electronics

1. Introduction

Flexible electronic devices such as flexible displays, electronic skins, and implantable devices, are gaining increasing attention for their portability, lightweight design, and adaptability to human use. (1-4) Ferroelectric field-effect transistors (FeFETs) are particularly promising for these applications due to their low power consumption, and high-speed operation. (5-7) However, mechanical strain may lead to a dielectric breakdown due to internal defect formation, posing a challenge to device reliability. (8)

Among the ferroelectric materials, fluorite-based films have gained significant attention because of their advantages such as environmental friendliness, large band gap, and simplified structure. (9) Zirconium oxide (ZrO₂) has been widely investigated due to its low crystallization temperature. (10,11) Note that the ferroelectric properties of ZrO₂ can be shown in wide thickness ranges with large process margins. (12) For flexible substrates, polyimide (PI) substrates are widely used for flexible displays because of their excellent mechanical and thermal stability and manufacturing capabilities. (1,3) Recent research has demonstrated the direct growth of HZO films on PI substrates for low-voltage nonvolatile transistors. (6) Additionally, PI can be combined with polydimethylsiloxane (PDMS) substrates to enhance mechanical properties, enabling the development of stretchable thin-film transistors (TFTs). (13)

The process compatibility with the conventional switching transistors is important for applying the FE devices. Previous research has demonstrated the fabrication of ferroelectric capacitors or transistors on CMOS backplanes. However, the complexity of this approach leads to an ongoing need for simplified and efficient fabrication methodologies. (14)

This work proposes a mechanically stable, metal-insulator-semiconductor-ferroelectric (MISF) structured ferroelectric thin-film transistor (FE-TFT) deposited by spray pyrolysis on PI and PDMS substrates. The spray-pyrolyzed ZrO₂ shows crystalline o-phase formation. The ferroelectric behavior of the device is achieved by ferroelectric coupling of the ZrO₂ layer. The TFT shows a large memory window (MW) of 9.1 V at ± 15 V gate voltage (VGS) sweep, with good temperature stability. The device could be operated well under 1 mm bending radius (R).

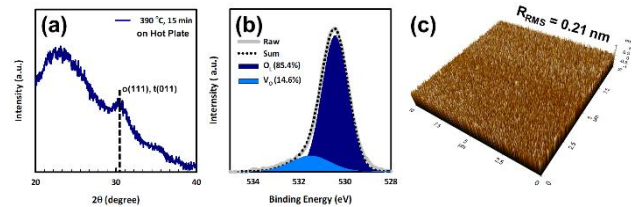


Figure 1. ZrO₂ thin film characterization. (a) The GIXRD spectra, (b) XPS O1s spectra, and (c) surface morphology by AFM measurements.

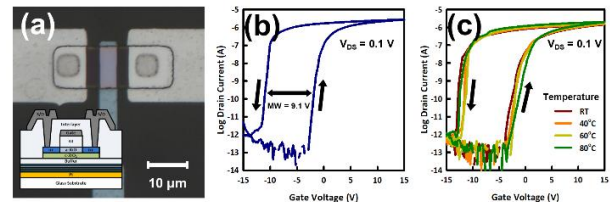


Figure 2. Electrical characterization of the FE-TFTs. (a) Optical image of the fabricated device with W/L of 10 $\mu\text{m}/6$ μm . The inset depicts the cross-sectional view of the FE-TFT. (b) The hysteresis curve at a ± 15 V V_{GS} sweep. (c) Hysteresis curve with various temperatures.

The TFTs were transferred onto PDMS substrates for stretchability. The stretchable TFT shows a stable operation for 100 h in a 30 % biaxially stretched condition. The 3T0C pixel circuit was made based on the MISF TFT. The switching oxide-TFTs (SW-TFTs) were made without the ferroelectric layer, with the MISF process. The 3T0C pixel circuit was used for the PWM mode of micro-LED displays. The proposed ferroelectric MISF TFTs could be used for next-generation, flexible, and stretchable display devices.

2. Experimental Section

A precursor solution of 0.15 M ZrO₂ was prepared by dissolving Zirconium (IV) acetylacetonate (Zr(C₅H₇O₂)₄, 97%) in a mixed solvent of Dimethylformamide (C₃H₇NO, $\geq 99.75\%$) and Methanol (CH₃OH, $\geq 99.9\%$) with 7:3 ratio. The precursor solution was prepared in an N₂ environment and stirred at 70 °C for 8 hrs. A 0.45 μm PTFE syringe filter was used to eliminate residual particles from the precursor solution before spray coating.

The fabrication process of flexible MISF FE-TFTs on polyimide substrate is as follows. First, the carbon nanotube/graphene oxide sacrificial layer was deposited by spray pyrolysis. Then, PI was coated to 10 μm and cured at 450 °C for 2 h. After the deposition of the gas barrier and buffer oxide layer consisting of SiO₂/SiN_x multilayer by plasma-enhanced chemical vapor deposition (PECVD) at 420 °C, a 30 nm thick ZrO₂ layer was deposited by spray pyrolysis at the temperature of 370 °C using a Lab Spray Coater (ReVo-S). During spray coating, the distance between the substrate and the spray nozzle was maintained at 10.0 cm, and the

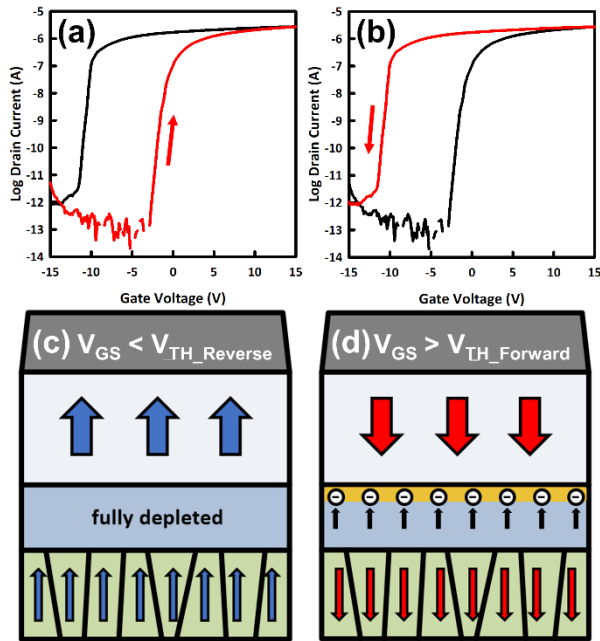


Figure 3. Operational mechanism of the proposed FE-TFTs. (a), (b) The hysteresis curves and (c), (d) carrier concentrations in the active layer and electrical force induced by the dipole orientation in FE layer.

nozzle's moving speed was set at 7.0 cm s^{-1} . The flow rate of precursor solution during spray remained constant at approximately 2.5 mL min^{-1} . The film was treated with 2 cycles of Ar/O₂ plasma and annealed on a hot plate at $390 \text{ }^\circ\text{C}$ for 15 mins in air. Then, 10 nm amorphous indium gallium oxide (a-IGO) was deposited at room temperature by sputtering as an active layer. A 100 nm thick SiO₂ and 100 nm thick Mo were deposited as a gate insulator (GI) and gate electrode by PECVD and sputtering, respectively. The doping region was formed by a self-aligned process utilizing a gate electrode as a photomask. A 300 nm thick SiO₂, and 150 nm thick Mo were deposited as interlayer and source/drain (S/D) electrodes, respectively. Finally, the TFTs were annealed in a vacuum furnace at $250 \text{ }^\circ\text{C}$ for 2 hrs.

The electrical characteristics of the FE-TFTs were analyzed by an Agilent 4156C semiconductor parameter analyzer. The threshold voltage (V_{TH}) was defined as the gate voltage (V_{GS}) corresponding to constant drain current (I_{DS}) of $W/L \times 10 \text{ pA}$ at drain voltage (V_{DS}) of 0.1 V, where W is channel width and L is length. The memory window was calculated by the difference of V_{TH} of the forward sweep ($V_{\text{TH_Forward}}$) and the reverse sweep ($V_{\text{TH_Reverse}}$) from the voltage sweeping hysteresis measurements. The μ_{FE} was calculated by transconductance; $\mu_{\text{FE}} = L/(WC_{\text{OX}}V_{\text{DS}}) g_{\text{m_max}}$, where C_{OX} is the capacitance of the gate dielectric and $g_{\text{m_max}}$ is the maximum transconductance.

3. Results and Discussion

The properties of ZrO₂ films by Ar/O₂ plasma treatment and sequent crystallization were analyzed. **Fig. 1(a)** shows the grazing incidence X-ray diffraction (GIXRD) spectra of the ZrO₂ film. The peak was shown at 30.4° indicating an orthorhombic phase formation in ZrO₂. (11) **Fig. 1(b)** shows the O1s spectra of X-ray photoelectron spectroscopy (XPS) resulting from the surface of the ZrO₂. The metal-oxygen bonds and the oxygen vacancies were calculated as 85.4% and 14.6 % respectively. The oxygen-related defects were effectively suppressed by Ar/O₂ plasma

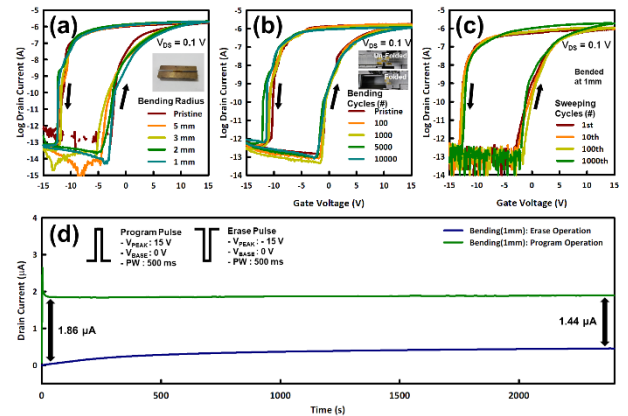


Figure 4. Mechanical stabilities of the FE-TFT. Hysteresis curves with (a) bending radius down to 1 mm, (b) bending tests up to 10000 cycles at $R = 3 \text{ mm}$, and (c) endurance measurements of up to 1000 times of $\pm 15 \text{ V}$ V_{GS} sweep at $R = 1 \text{ mm}$. (d) Retention characteristics measured up to 2400 s at $R = 1 \text{ mm}$. The insets show the pulse conditions for the program and erase pulses.

Table 1. The comparison of the structural and mechanical properties of flexible FE-TFTs.

Structure	Deposition Method	Ferroelectric Material	Flexible Substrate	Minimal Bending Radius	Year (Ref.)
MFS	ALD	Hf _{0.5} Zr _{0.5} O ₂	MICA	4 mm	2020 (5)
MFIS	Spin Coating	Hf _{0.5} Zr _{0.5} O ₂	PI	2 mm	2022 (6)
MFS	ALD	Hf _{0.5} Zr _{0.5} O ₂	MICA	5 mm	2024 (7)
MISF	Spray Pyrolysis	ZrO ₂	PI	1 mm	This Work

treatment. (15) The root-mean-square surface roughness (R_{RMS}) of 0.21 nm by the atomic force microscopy (AFM) measurements are shown in **Fig. 1(c)**.

Fig. 2(a) shows an optical image of MISF TFT. The electrical characteristics were measured with the TFT of $W = 10 \text{ }\mu\text{m}$ and $L = 6 \text{ }\mu\text{m}$. The inset shows the cross-sectional view of the MISF TFT. **Fig. 2(b)** shows a counter-clockwise hysteresis curve measured with $MW = 9.1 \text{ V}$ at a $\pm 15 \text{ V}$ V_{GS} sweep. The drain voltage (V_{DS}) of 0.1 V was used for the measurement to minimize the drain bias effect which can affect the dipole orientation. **Fig. 2(c)** shows hysteresis curves with rising temperatures of up to $80 \text{ }^\circ\text{C}$. The $V_{\text{TH_Forward}}$ tends to shift slightly in a positive direction indicating some charge trapping. (15)

The operational mechanism is depicted in **Fig. 3**. **Fig. 3(a) and (b)** highlight the forward and reverse sweep respectively. **Fig. 3(c) and (d)** show the ferroelectric dipole orientation and carriers in the active layer. By ferroelectric coupling, the dipoles can induce repulsive/attractive force to the charge carriers, and affect the carrier concentration at the channel region. (16,17) The forward sweep operation is first induced with the negative voltage, orienting the dipoles to induce attractive force to the electrons forcing them to be fully depleted as shown in **Fig. 3(c)**. The reverse sweep is vice versa, inducing repulsive force from the ferroelectric dipoles making the electrons accumulate at the interface as shown in **Fig. 3 (d)**. (16,17) The device operates without forming a direct leakage current path through the ferroelectric layer. This can also improve the stability of the

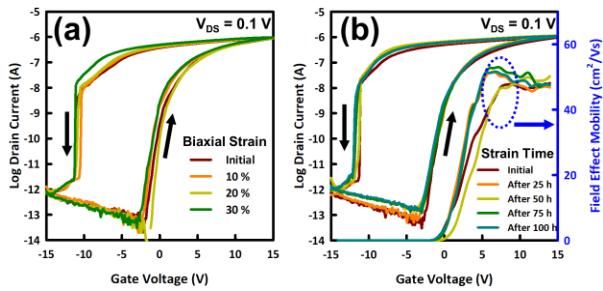


Figure 5. The stretchability of the FE-TFT on PI/PDMS substrate. Hysteresis curves of (b) the stretched FE-TFT up to 10% to 30% and (c) up to 100 h with the fixed biaxial strain of 30 %.

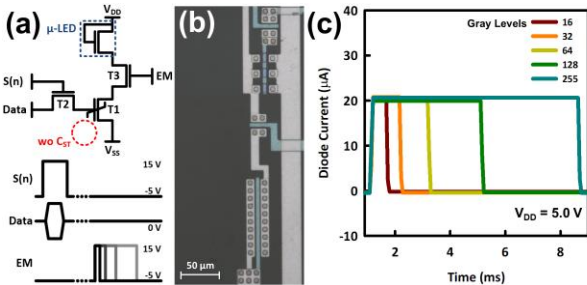


Figure 6. Display pixel application of the FE-TFT. (a) Pixel circuit and timing diagram of the 3T0C pixel with the FE-TFT working as a constant current part. (b) Optical image of the 3T0C circuit with the W/L = 30/6 μm of driving FE-TFT and W/L = 20/6 μm of SW-TFT. (c) The current measurement of the 3T0C pixel circuit

device. (16,17)

Bending and stretching tests were conducted on the FE-TFT to evaluate the mechanical stability. **Fig. 4(a)** shows hysteresis curves of the flexible FE-TFT of R = 5 mm, 3 mm, 2 mm, and 1 mm. **Fig. 4(b)** depicts hysteresis curves with 10000 cycles (R = 3 mm) of bending endurance. The device showed stable operation in both bending tests. The endurance and retention characteristics at R = 1 mm are shown in **Fig. 4(c)** and **(d)**, respectively. The endurance shows stable operation of up to 1000 cycles at a ± 15 V V_{GS} sweep. The retention characteristics show a slight increase in current, due to the depletion nature of the device. (17) **Table 1** summarizes the reported fluorite-based flexible FE-TFTs. The proposed device shows the lowest operable bending radius. The FE-TFTs on the PI substrate were transferred onto the PDMS substrate to achieve stretchability. The detailed PDMS transfer process flow is demonstrated in our previous work. (13) The stretchability of the device was evaluated with the biaxial stretching test up to 30 % (**Fig. 5(a)**) and by maintaining 30 % biaxial strain for 100 h (**Fig. 5(b)**). The $\Delta\mu_{FE}$ showed a maximum of 7.9 % compared to the initial state, indicating the mechanical robustness of the FE-TFTs.

Fig. 6 shows the possible display application of the FE-TFT. **Fig. 6(a)** shows a circuit diagram of the proposed pixel circuit. The driving FE-TFT (T1) was utilized as the constant current generation (CCG) using the memory characteristics. SW-TFTs (T2, T3) were fabricated by removing the ferroelectric layer before active deposition. **Fig. 6(b)** shows the optical image of the fabricated 3T0C pixel circuit. The pulse width modulation (PWM) operation is displayed in **Fig. 6(c)**. The pulse width was modulated with a single EM transistor at this level. The current

showed 20 μA of on-current at $V_{DD} = 5.0$ V, and the current was maintained throughout the measurements. Note that the current was maintained constantly without a storage capacitor. Although challenges remain in achieving individual pixel operation, the results demonstrate the possibility of FE-TFT replacing CCG components in PWM pixel circuits.

4. Conclusion

We proposed an MISF-structured FE-TFT on flexible & stretchable substrates. The FE-TFT showed 9.1 V of MW with ± 15 V V_{GS} sweep. The device operates by ferroelectric coupling without having the leakage current path through the FE layer. Mechanical tests confirmed robustness, with stable operation at R = 1 mm. The device maintained $\Delta\mu_{FE} < 7.9\%$ under 30% biaxial strain for 100 h, validating its stretchability. Further, the 3T0C pixel circuit is proposed using the MISF device. The SW-TFTs were realized by etching the FE layer during the MISF process. The current remained stable throughout the measurements, suggesting the potential for replacing the CCG component in PWM pixel circuits.

5. Acknowledgements

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